

# Effect of Organic Loading on Hydrogen in A Continuous Bio-hydrogen Production Reactor

Li Ning<sup>#1</sup>, Li Yongfeng<sup>#\*2</sup>, Wang Bing<sup>#3</sup>, Gao Miao<sup>#</sup>, Han Tianxue<sup>#5</sup>, Zhang Lingling<sup>#6</sup>

<sup>#</sup>Forestry School, Northeast Forestry University, Harbin 150040, China

<sup>\*</sup>Chemical School, Shanghai University of Engineering Science, Shanghai 201620, China

<sup>1</sup>huanjinglining@163.com; <sup>2</sup>dr\_lyf@163.com; <sup>3</sup>734477706@qq.com;

<sup>4</sup>724160005@qq.com; <sup>5</sup>530459363@qq.com; <sup>6</sup>1046651283@qq.com

**Abstract**—This experiment used a continuous stirred tank reactor (CSTR) with brown sugar water as the fermentation substrate, and sewage sludge as the initiation of reaction. Hydrogen production reached a stable level under conditions of an intake of pH  $7.0 \pm 0.1$ , an oxidation-reduction potential (ORP) of  $-420\text{mV}$ , a temperature of  $(35 \pm 1)^\circ\text{C}$ , and a hydraulic retention time (HRT) of 6 hours. (Hydrogen was the main component from the ethanol-type fermentation). We were able to focus on the impact of changing the organic load on Hydrogen production by keeping all other parameters consistent. At the same time, the microorganisms were allowed to maintain high activity by regulating the pH level. Results showed that when the organic load increased from  $12\text{ kg/m}^3\text{-d}$  to  $32\text{ kg/m}^3\text{-d}$ , the biogas and hydrogen production rates continuously increased. When the organic load was  $32\text{ kg/m}^3\text{-d}$ , it reached a maximum production rate of  $18.6\text{L/d}$  and a hydrogen production rate of  $6.4\text{L/d}$ . Compared with the initial  $12\text{ kg/m}^3\text{-d}$ , gas production improved by 89% and 87%, respectively. During system operation, lowering the intake pH to 5.85 resulted in the inhibition of microbial activity of anaerobic fermentation, resulting in a decline of rate of hydrogen production and the ORP increased to  $-328\text{mV}$ . Under these conditions, the reactor could maintain a high hydrogen production rate of ethanol-type fermentation by adding a certain amount of NaOH in the reactor to regulate the pH level.

**Keywords**— CSTR; pH; Hydrogen Production; Organic Loading; Ethanol-Type Fermentation

## I. INTRODUCTION

With the extensive use of fossil fuels such as coal and oil, the earth has seen an increase in serious pollution of the global environment. This pollution has been posing a threat to human survival. Additionally, fossil fuels are non-renewable energy source. Therefore, development and application of alternative source of energy, hydrogen has attracted extensive attention. It is also one of the most promising clean energies of the future energy structure and it will play an important role in the field of energy for its excellent and useful performance.

It is of great strategic significance that hydrogen energy is developed in China. As a matter of fact, it plays a real important role in developing energies for bio-hydrogen production technology<sup>[1]</sup>. Continuous-flow stirred tank reactor (CSTR) with mechanical mixing and high mass efficiency can

boost hydrogen production efficiency. Additionally, this method that requires a relatively simple device and technology can significantly reduce the cost of bio-hydrogen production, resulting in the realization of the industrialized production of hydrogen gas<sup>[1, 2, 3]</sup>. This article studies the effect of organic load on an anaerobic bio-hydrogen system, which provides a theoretical basis for achieving the rapid degradation of organic wastewater and the production of hydrogen energy.

## II. MATERIAL AND METHODS

### A. Experimental facility

This experiment used continuous-flow stirred tank reactor (CSTR) with an effective volume of  $7.0\text{L}$  and a total volume of  $19.4\text{L}$ . The reactor with agitator realized that microorganisms can be completely mixed with intake water by mixing (at speeds of  $120\text{r}\cdot\text{min}^{-1}$ ). There is a gas-liquid-solid three-phase separator inside the reactor and it has an integrated structure of reaction and sedimentation zones. Locked with water through the shaft, the reactor was under anaerobic conditions. The temperature was automatically controlled at the level of  $(35 \pm 1)^\circ\text{C}$  with resistance wire around the reactor wall, which guaranteed high activity of micro-organisms. The structure of continuous-flow mixing reactor is shown in Figure 1.

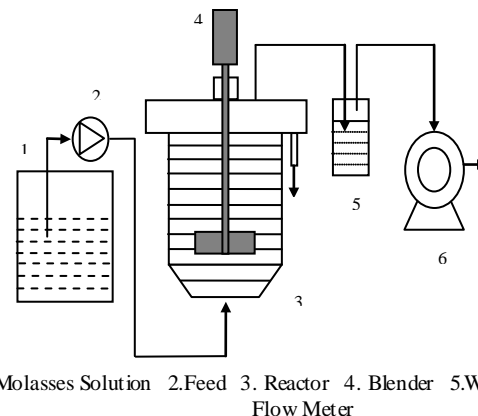


Fig.1 Schematic diagram of CSTR

### B. Analytical Methods

The biogas composition including hydrogen and carbon dioxide was measured by using a gas chromatograph (GC, 6809N Network GC System, Agilent Technologies, Waldron, Germany) equipped with a thermal conductivity detector (TCD). The column (2m\*5mm) was filled with porapak Q (50-80 meshes), Nitrogen was used as carrier gas with a flow rate of 40 mL/min and Methane was not detected in the biogas.

CODs of the samples were measured according to Standard Methods<sup>[4]</sup>. The pH and ORP were measured by pH meter (PHS-25). A wet gas meter (LML-1) was utilized to measure biogas yield.

Volatile fatty acids (VFA) and ethanol in liquid samples were measured by using a gas chromatograph (GC, 6890N Network GC System, Agilent Technologies, Waldbrown, Germany) equipped with a flame ionization detector (FID). The column (Zm) was packed with supporter of GDX-103 (60-80 meshes). The temperatures of the injection part, the oven, and the detector were adjusted to 220°C, 190°C, and 220°C, respectively. The carrier gas was nitrogen at a flow rate of 30mL/min also.

### C. Sludge acclimation and run controlled parameters

The experiment used inoculation sludge from secondary sedimentation tanks of a certain sewage treatment plant in Harbin. The debris and particulate matter could be removed by being precipitated, washed, and filtered. Used brown sugar with a COD of 10000mg/L and added an amount of N and P-fertilizer, COD, N, and P had a mass ratio of 1000:5:1, which ensured that the sludge micro-organisms met N and P nutrient needs during the growth. The sludge was cultivated with intermittent aeration for 20 days. During the process, aeration was stopped for 1 hour, rested, while the upper liquid was extracted and clean water was added on a daily basis. The mature sludge presented brown, granular and settled well after domestication.

The well domesticated sludge was turned into the hydrogen production reactor. Under the conditions of hydrogen retention time (HRT) 6 hours, temperature ( $35 \pm 1$ ) °C, intake pH  $7.0 \pm 0.1$ , organic load  $12 \text{ kg/m}^3\text{-d}$ , suspended solid (SS)  $12.93 \text{ g/L}$ , Volatile suspended solids (VSS)  $8.46 \text{ g/L}$ , VSS/SS (biological activity) 0.65, the reactor started with a continuous flow way. After about 30 days, it reached a stable state. At this point, the gas production was up to  $2.0 \text{ L/d}$ , hydrogen accounted for about 41%, pH of wastewater was around 5.0, ORP was -420mV. The average concentrations of fermentation products (including small molecular fatty acids and alcohols) were: ethanol  $280 \text{ mg/L}$ , acetic acid  $63 \text{ mg/L}$ , propionic acid  $66 \text{ mg/L}$ , butyrate acid  $87.5 \text{ mg/L}$  and valeric acid  $6 \text{ mg/L}$ . Among them, ethanol and acetic acid accounted for 68.26 %, which meant becoming the ethanol-type fermentation.

After stability, anaerobic activated sludge fermentation system kept the hydraulic retention time unchanged (HRT=6h) in operation process. By increasing organic load and adjusting intake pH, we studied its impact on CSTR reactor for hydrogen production capacity. The running process in which organic load increased from  $12 \text{ kg/m}^3\text{-d}$  to  $32 \text{ kg/m}^3\text{-d}$  was divided into six stages, each stage increased  $4 \text{ kg/m}^3\text{-d}$  and response (run) time was 6 days.

## III. RESULTS AND ANALYSIS

### D. Changes of Biogas, hydrogen production rates

As is shown in Figure 2, in the process of the intake organic load increased from  $12 \text{ kg/m}^3\text{-d}$  to  $28 \text{ kg/m}^3\text{-d}$  gradually. The gas production rate witnessed a trend of sustained growth and the increasing rate of hydrogen production changed marginally. The hydrogen content varied from 22.9% to 50.4%. At each stage, the total gas production rates sometimes slightly dropped after the upgrade of the organic load, but hydrogen production rate remained stable without obvious changes. It was possibly because microorganisms other than the hydrogen-producing bacteria lacked the tolerant capacity of load impact and their activity declined, which caused a reduction in carbon dioxide and other gases<sup>[10]</sup>. In the next day after the organic load rose to  $32 \text{ kg/m}^3\text{-d}$ , biogas production rate reached the highest point at  $18.6 \text{ L/d}$  and hydrogen production rate peaked at  $6.4 \text{ L/d}$ , hydrogen content was 34.4% at this moment. Compared with initial organic load  $12 \text{ kg/m}^3\text{-d}$ , the biogas and hydrogen production rates increased 89% and 87%, respectively. Although in the following few days, all the three items mentioned above experienced a slight drop, there were still relatively high levels of gas production rates and hydrogen content. This phenomenon may be due to hydrogen-producing fermentation microorganisms need a process of adaptation to high organic load. High load impact within a short time coupled with the increasing yield of liquid fermentation of volatile acids made the biological activity inhibited and organic catabolic rate dip slightly. As can be seen from the graph, the microorganisms rapidly adapted to the environment of high organic load in the next two days and the gas production rates rebounded. Worth noticing is, it was low pH that caused the decline of gas production rates when organic load stood at  $20 \text{ kg/m}^3\text{-d}$ . However, hydrogen production rate barely changed, which showed hydrogen-producing bacteria had the tolerant capacity of pH to a certain extent<sup>[8]</sup>.

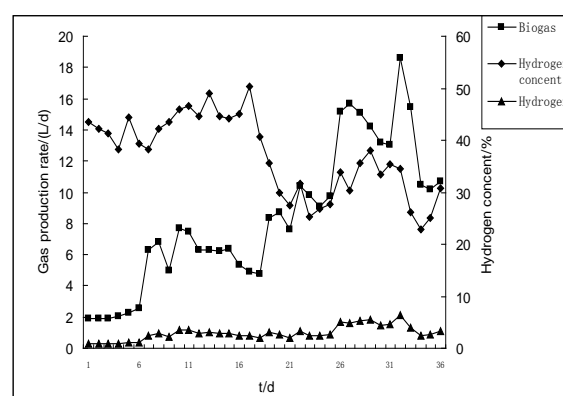


Fig.2 Changes of biogas and hydrogen gas in operation process of the reactor

### E. Changes of pH

pH is an essential ecological element which could affect different hydrogen-producing fermentations<sup>[6,9]</sup>. The activity of enzymes which participate in metabolic processes will be directly affected by variations of pH. Under different pH conditions, different kinds of bacteria grow at distinguishing

speeds, which influence changes of microbial populations and communities in the biological hydrogen-producing reactor ultimately, thereby change the number and position of dominant populations and cause changes of fermentation types. Most fermentative hydrogen production is operated under acidic conditions which could inhibit the activity of methanogenic bacteria and help degradation of the organic load to be maintained in hydrogen-producing stage. Figure 3 reflects water pH fluctuation of entire process in the reactor. Numerous studies showed that the optimum pH was between 5.0 and 6.0. In this study, when the organic load amounted to  $12\text{kg/m}^3\text{-d}$  -  $16\text{kg/m}^3\text{-d}$ , the outlet pH could be regulated to approximately 5.0 by adding a certain amount of NaOH to the intake. When the organic load increased from  $20\text{kg/m}^3\text{-d}$  to  $28\text{kg/m}^3\text{-d}$ , stopped adding NaOH and the intake pH plummeted to around 5.85. The sudden decrease of pH affected microbial enzyme activity which gave rise to a downward trend of the metabolic rates and outlet pH declined to roughly 4.3 as well. Micro-organisms gently adapted to the intake pH changes, metabolic rate rocketed and outlet pH reached a plateau at about 4.6 when the organic loading arrived at  $24\text{kg/m}^3\text{-d}$ .

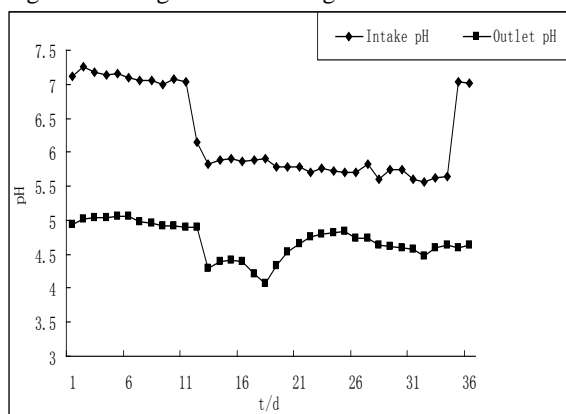


Fig.3 Changes of pH in operation process of the reactor

#### F. Changes of oxidation-reduction potential (ORP)

ORP is also an ecological factor of overriding importance. In the hydrogen fermentation process, low oxidation-reduction potential is a necessary condition for the growth of hydrogen-producing fermentation microorganisms [7]. This is because only the low ORP environment is suitable for anaerobic microorganisms' survival requirements. Some of them including Coenzyme I, Ferredoxin and Flavoprotein, etc—the dehydrogenase system require low ORP environment to maintain activity. During the entire operating process, the system ORP changed between  $-430\text{mV}$  and  $-328\text{mV}$ , as shown in figure 4. ORP was mainly implicated by the changes of pH and we can discern from figure 3 and figure 4, ORP and pH were negatively correlated. When the pH lowered, the hydrogen-producing fermentation microbial activity was inhibited; changes of hydrogen-producing fermentation environment in system caused an increase in ORP. During the 1 to 12 days, ORP had no evident fluctuation, peaking at  $-328\text{mV}$  on the eighteenth day and then decreased steadily, leveled off at  $-390\text{mV}$ , eventually.

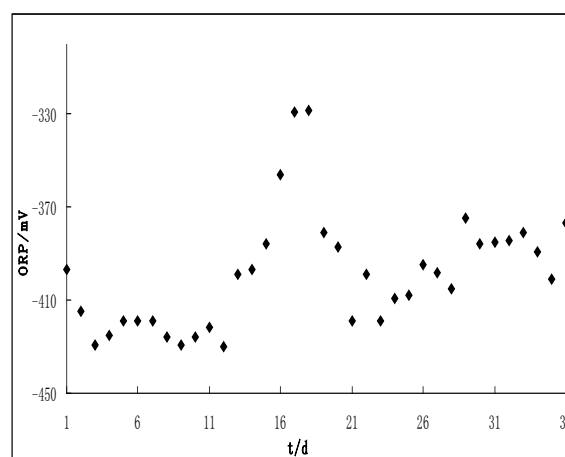


Fig.4 Changes of ORP in operation process of the reactor

#### G. Changes of liquid terminal products

Figure 5 reflects changes of liquid terminal products by the anaerobic activated sludge ferment produce hydrogen system in the whole operation process. With the continual increase of the organic load of intake water, the total content of liquid terminal fermentation products kept increasing, from  $506.7\text{mg/L}$  of the initial organic loading  $12\text{kg/m}^3\text{-d}$  to  $1376.2\text{mg/L}$  of organic load  $32\text{kg/m}^3\text{-d}$ . Ethanol increased more obviously than other liquid terminal products when the volatile acids fluctuated. From the 15<sup>th</sup> to 30<sup>th</sup> day, the activity of acidogenic fermentation microorganisms was controlled by the low pH. At the same time, the content of ethanol and acetic acid decreased apparently, dropping from  $603.8\text{mg/L}$  and  $283.5\text{mg/L}$  to  $327.0\text{mg/L}$  and  $134.7\text{mg/L}$ , respectively. When the organic loading increased from  $28\text{kg/m}^3\text{-d}$  to  $32\text{kg/m}^3\text{-d}$ , the dominant butyrate gave priority to volatile acid. At this point, both the ethanol-type fermentation and butyric acid type fermentation existed, but the ethanol-type played the dominant role [12]. As the intake organic load increasing from  $12\text{kg/m}^3\text{-d}$  to  $32\text{kg/m}^3\text{-d}$  in the whole reaction system, the total content of liquid terminal fermentation products in the various stages represented  $506.7$ ,  $730.4$ ,  $860.4$ ,  $975.5$ ,  $274.6$ ,  $1376.2\text{mg/L}$  while the content of ethanol and acetic acid were  $346.8$ ,  $499.4$ ,  $646.1$ ,  $757.7$ ,  $935.4$ ,  $1012.447\text{mg/L}$ , which respectively accounted for  $68.4\%$ ,  $68.4\%$ ,  $75.1\%$ ,  $77.7\%$ ,  $73.4\%$ ,  $73.6\%$  of the total. From the above data, we came to the conclusion: although the conditions such as water pH, organic load, ORP and so on changed in various degrees, the system remained ethanol-type fermentation all the time.

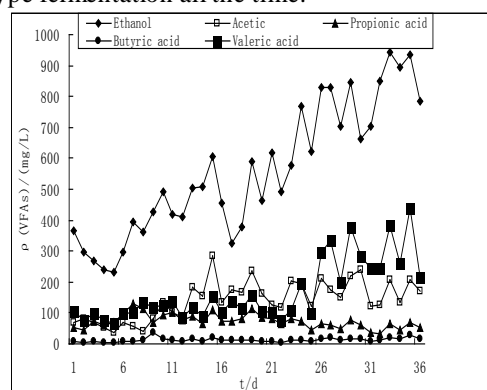


Fig.5 Changes of concentration of fermentation liquid products in operation process

### H. Changes of COD degradation rate

Figure 6 showed changes of intake and outlet COD concentration and COD degradation rate in the whole system. The variation trend of intake COD concentration was almost the same with the outlet; COD degradation rate changed between 34.8% and 57.2%. In the traditional way of anaerobic wastewater treatment, COD was dislodged mainly by the way that the methanogens change the intermediate products into methane. While in single-phase CSTR reactor, it was hydrogen-producing acidogenic bacteria that played a dominant role; COD was degraded by hydrolysis and aerogenesis, and was converted into organic acid of liquid terminal products. Therefore, the degradation rate cannot be high<sup>[5]</sup>.

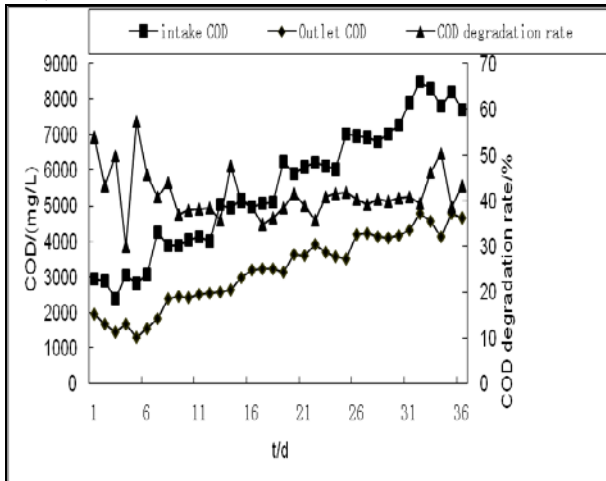


Fig.6 Changes of COD degradation rate in operation process of the reactor

### IV. CONCLUSIONS

From this study, we draw a conclusion that it is better to control the continuous stirred tank reactor (CSTR) with an intake of pH  $7.0 \pm 0.1$ , an oxidation-reduction potential (ORP) of  $-420\text{mV}$ , a temperature of  $(35 \pm 1)^\circ\text{C}$ , a hydraulic retention time (HRT) of 6 hours. Under these conditions, while intake of organic load increased from  $12\text{kg}/\text{m}^3\text{-d}$  to  $32\text{kg}/\text{m}^3\text{-d}$ , the hydrogen production capacity of anaerobic activated sludge continued to rise. When the organic load stood at  $32\text{kg}/\text{m}^3\text{-d}$ , the maximum biogas and hydrogen production rate reached  $18.6\text{L}/\text{d}$  and  $6.4\text{L}/\text{d}$ . When compared with organic load  $12\text{kg}/\text{m}^3\text{-d}$ , they improved 89% and 87%, respectively.

Hydrogen-producing bacteria have better tolerant capacity of high organic load on a brown sugar effluent. They can quickly adapt to the changing environment of high organic load in a short time, and then reach a steady production of hydrogen. In this test, when the organic load was  $20\text{kg}/\text{m}^3\text{-d}$ , as not adjusting the intake pH, anaerobic activated sludge microorganisms were unable to adapt to environmental changes caused by low pH. As a result, its activity was stifled, biogas and hydrogen production rates all declined. At this moment, ORP reached the highest point at  $-328\text{mV}$ . Therefore, as intake COD concentration increasing, it's better to add a certain amount of NaOH into the reactor to regulate pH and ensure that hydrogen fermentation of micro-organisms have higher activity. Meanwhile, stability of ethanol-type fermentation is maintained and a higher rate of stable hydrogen production is realized.

### REFERENCES

- [1] R.S. Prakasham, P. Brahmaiah, T. Sathish, et al. Fermentative biohydrogen production by mixed anaerobic consortia: Impact of glucose to xylose ratio[J]. International Journal of Hydrogen Energy, 2009, 34(23): 9354-9361.
- [2] Li Y F, Ren N Q, Chen Y et al. Ecological mechanism of fermentative hydrogen production by bacteria[J]. International Journal of Hydrogen Energy, 2007, 32(7): 755-760.
- [3] N.Q. Ren, B.Z. Wang and J.L. Hung. Ethanol-type fermentation from carbohydrate in high rate acidogenic reactor[J]. Biotechnol Bioeng, 1997, 54: 197-200.
- [4] APHA. Standard Methods for the Examination of Water and Wastewater. 19th. [J]. American Public Health Association, Washington, DC, 1995.
- [5] F.R. Hawkes, R. Dinsdale, D.L. Hawkes, et al. Sustainable fermentative hydrogen production: challenges for process optimisation [J]. International Journal of Hydrogen Energy, 2002, 27(11-12): 1339-1347.
- [6] LI Yong-feng, HAN Wei, XU Jing-li, CHEN Hong, WANG Lu, Chuan-ping. International Conference on Biomass Energy Technologies: Dec 3-5(2008), p855.
- [7] Shuang Gao, Bing Wang, Lei-lei Zhu, Wei Han, Hong Chen, Yong-feng Li. Effect of organic loading rate on fermentative hydrogen production in CSTR: Advanced Materials Research Vols. 156-157.
- [8] Pinto FAL, Troshin O, Lindblad P. A brief look at three decades of research on cyanobacterial hydrogen evolution. Int J Hydrogen Energy 2002; 27: 1209-15.
- [9] Lee MJ, Zinder SH. Hydrogen partial pressures in a thermophilic acetate-oxidizing methanogenic co-culture. Appl Environ Microbiol 1988; 54: 1457-61.
- [10] Van Niel EWJ, Claassen PAM, Stams AJM. Substrate and product inhibition of hydrogen production by the extreme thermophile Caldicellulosiruptor saccharolyticus. Biotechnol Bioeng 2002; 81: 255-62.
- [11] Hawkes FR, Dinsdale R, Hawkes DL, Hussy I. Sustainable fermentation hydrogen production: challenges for process optimization. Int J Hydrogen Energy, 27, 1339-47, 2002.
- [12] Bai M D, Chang S M, Wu K L, Chen W C. Feasibility Study of Hydrogen Production with Anaerobic Digestion of Pretreated Sludge [A]. Proceeding of 9<sup>th</sup> International Conference on Anaerobic Digestion, 2001, 245-247.